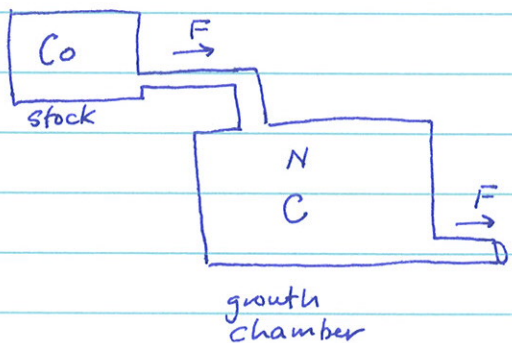


Uniton Dimensional Analysis Chemostat

LEK p121-129

Device for sustained growth of bacteria



$C_0 =$  conc of stock solution of nutrient

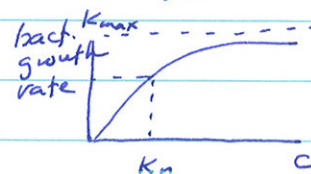
$C(t) =$  conc nutrient in growth chamber

$N(t) =$  " bacteria

adjustable parameters:  $C_0$ , also  $F =$  flow rate  
 $V =$  volume of growth chamber

$$\begin{cases} \frac{dN}{dt} = K(C)N - \frac{FN}{V} \\ \frac{dC}{dt} = -\alpha K(C)N - \frac{FC}{V} + \frac{FC_0}{V} \end{cases}$$

$$K(C) = \frac{K_{max}C}{K_n + C}$$



Dimension carrying eqns:

$$\begin{cases} \frac{dN}{dt} = \frac{K_{max}C}{K_n + C} N - \frac{FN}{V} \\ \frac{dC}{dt} = -\alpha \frac{K_{max}C}{K_n + C} N - \frac{FC}{V} + \frac{FC_0}{V} \end{cases}$$

Units	$N$	:	mass/vol	$gm/cm^3$
	$C$	:	mass/vol	$gm/cm^3$
	$F$	:	vol/time	$cm^3/s$
	$V$	:	vol	$cm^3$
	$K_{max}$	:	1/time	$1/s$
	$K_n$	:	mass/vol	$gm/cm^3$
	$\alpha$	:	—	— (dimensionless)

Transform system to Dimensionless form:

Let  $t = \tau \hat{t}$  dimension-carrying scales to be chosen

$N = \bar{N} \hat{N}$

$c = \bar{c} \hat{c}$  dimensionless variables

original variables ↑

Notation: in LER's book,  $\tau$ 's were used for the dimensionless var, and  $\wedge$  for choices of scales. Avoid confusion!

Rewrite eqns in terms of  $\wedge$  (dimensionless) variables.

$$\left\{ \begin{aligned} \frac{d(\bar{N}\hat{N})}{d(\tau\hat{t})} &= \frac{K_{max} \bar{c}\hat{c}}{K_n + \bar{c}\hat{c}} (\bar{N}\hat{N}) - \frac{F}{V} (\bar{N}\hat{N}) \\ \frac{d(\bar{c}\hat{c})}{d(\tau\hat{t})} &= -\alpha \frac{K_{max} (\bar{c}\hat{c})}{K_n + (\bar{c}\hat{c})} (\bar{N}\hat{N}) - \frac{F}{V} (\bar{c}\hat{c}) + \frac{F c_0}{V} \end{aligned} \right.$$

$$\left\{ \begin{aligned} \frac{\bar{N}}{\tau} \frac{d\hat{N}}{d\hat{t}} &= K_{max} \frac{\hat{c}}{(\frac{K_n}{\bar{c}}) + \hat{c}} \bar{N}\hat{N} - \frac{F}{V} \bar{N}\hat{N} \\ \frac{\bar{c}}{\tau} \frac{d\hat{c}}{d\hat{t}} &= -\alpha K_{max} \frac{\hat{c}}{(\frac{K_n}{\bar{c}}) + \hat{c}} \bar{N}\hat{N} - \frac{F}{V} \bar{c}\hat{c} + \frac{F c_0}{V} \end{aligned} \right.$$

$$\left\{ \begin{aligned} \frac{d\hat{N}}{d\hat{t}} &= \tau K_{max} \frac{\hat{c}}{(\frac{K_n}{\bar{c}}) + \hat{c}} \hat{N} - \frac{\tau F}{V} \hat{N} \\ \frac{d\hat{c}}{d\hat{t}} &= -\tau \alpha K_{max} \frac{\hat{c}}{\bar{c}} \frac{\hat{c}}{(\frac{K_n}{\bar{c}}) + \hat{c}} \hat{N} - \frac{\tau F}{V} \hat{c} + \frac{\tau F c_0}{V \bar{c}} \end{aligned} \right.$$

Now chose 'scales' for convenience: let  $\tau = V/F$ ,  $\bar{c} = K_n$ ,

$$\bar{N} = \frac{\bar{c}}{\tau \alpha K_{max}} = \frac{F K_n}{V \alpha K_{max}}$$

$$\begin{cases} \frac{d\hat{N}}{dt} = \alpha_1 \frac{\hat{C}}{1+\hat{C}} \hat{N} - \hat{N} \\ \frac{d\hat{C}}{dt} = -\frac{\hat{C}}{1+\hat{C}} \hat{N} - \hat{C} + \alpha_2 \end{cases} \quad \alpha_1 = \frac{\gamma K_{max}}{F} = \frac{V K_{max}}{F}$$

$$\alpha_2 = \frac{\gamma F C_0}{V \bar{C}} = \frac{C_0}{K_n}$$

We could now drop the  $\hat{\cdot}$ 's and arrive at:

$$\begin{cases} \frac{dN}{dt} = \alpha_1 \left( \frac{C}{1+C} \right) N - N \\ \frac{dC}{dt} = -\left( \frac{C}{1+C} \right) N - C + \alpha_2 \end{cases}$$

This is the dimensionless system, whose behaviour is seen to be determined by just two parameters,  $\alpha_1, \alpha_2$ .

### Analysis:

Nullclines:

$$\frac{dN}{dt} = 0 \quad \text{at} \quad \alpha_1 \left( \frac{C}{1+C} \right) N - N = 0 \Rightarrow N=0 \quad \text{or} \quad \alpha_1 \frac{C}{1+C} = 1 \Rightarrow \alpha_1 C = 1+C \Rightarrow C(\alpha_1 - 1) = 1 \Rightarrow C = \frac{1}{\alpha_1 - 1}$$

Conclusion Need  $\alpha_1 > 1 \Rightarrow \frac{V K_{max}}{F} > 1$  or  $F < V K_{max}$   
(flow rate should not be too fast)

Nullclines  $\frac{dC}{dt} = 0$  at  $-\left( \frac{C}{1+C} \right) N - C + \alpha_2 = 0$

- if  $N=0$  then  $C = \alpha_2 \Rightarrow SS (N_{ss}, C_{ss}) = (0, \alpha_2)$

This is undesirable for a chemostat where it is desired to have  $N_{ss} > 0$  i.e. to keep culture going.

- otherwise  $N = \frac{(1+C)}{C} (\alpha_2 - C)$   
 $\Rightarrow N = \left( \frac{1}{C} + 1 \right) (\alpha_2 - C)$

in this case (from before  $c_{ss2} = \frac{1}{\alpha_1 - 1}$ )

$$N_{ss2} = \left( \frac{\alpha_1 - 1}{1} + 1 \right) \left( \alpha_2 - \frac{1}{\alpha_1 - 1} \right) = \alpha_1 \left( \alpha_2 - \frac{1}{\alpha_1 - 1} \right)$$

SS(2)  
N<sub>ss2</sub>, C<sub>ss2</sub>

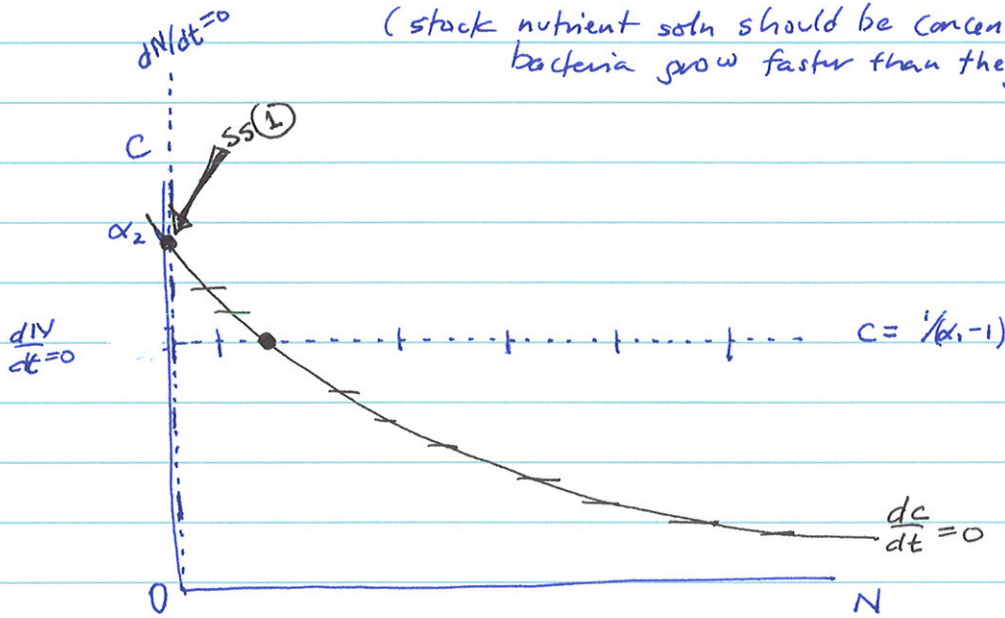
Conclusion (2): to have N<sub>ss</sub> > 0 need  $\alpha_2 > \frac{1}{\alpha_1 - 1}$

i.e.  $\frac{C_0}{K_n} > \frac{1}{V K_{max} - F}$

$$C_0 > \frac{K_n F}{V K_{max} - F}$$

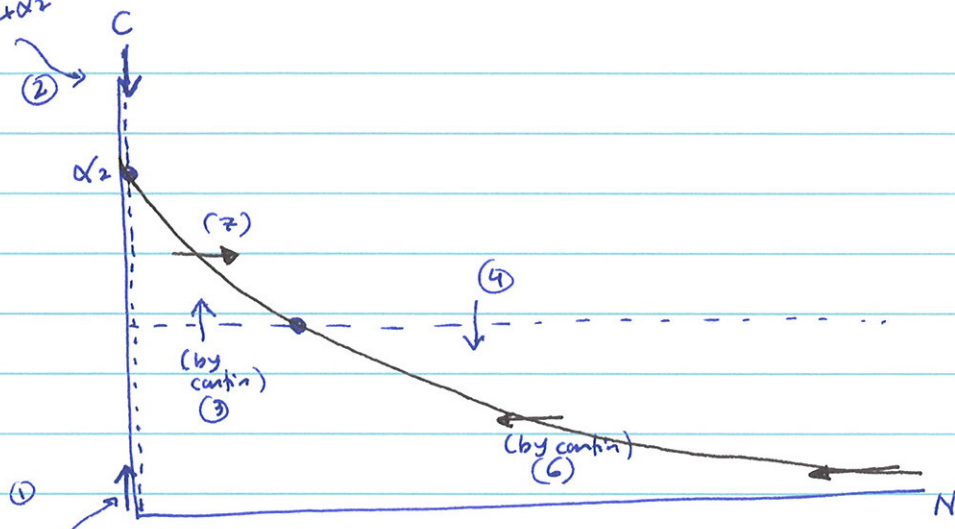
(stock nutrient soln should be concentrated enough to have bacteria grow faster than they get washed out)

p195  
LEK



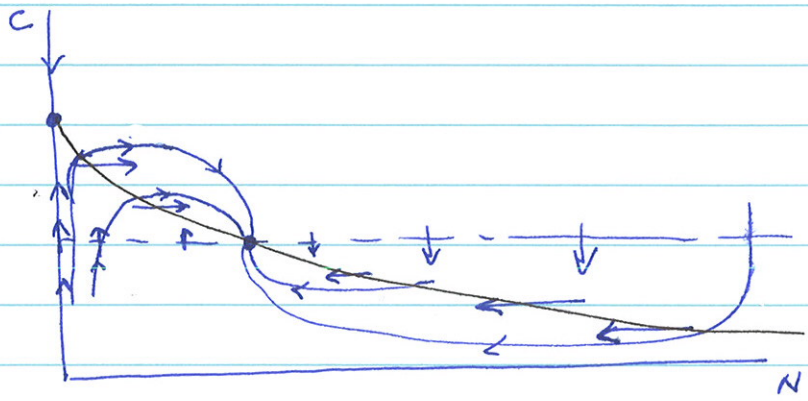
proper configuration when the conditions in  $\square$  are satisfied.

for large  $C$   
and  $N=0$   
 $\frac{dC}{dt} \approx -C + \alpha_2$



①  
close to  
 $(0,0)$   
 $\frac{dC}{dt} \approx \alpha_2 > 0$

⑤  
for  $C$  very small  
 $\frac{dN}{dt} \approx -N$



## Exercises - Chemostat

- (1) Draw a phase-plane diagram for the case where the chemostat "washes out" i.e. when the flow rate is too fast.
- (2) Selection of problems 10 - 13 on p 202-203 in LEK.  
(attached)

e.g.

Show that there is always a single stable S.S. and that there will not be any oscillations in the approach to that S.S.

- (3) Create an XPP ode simulation of the chemostat, showing phase plane behaviour. (Reasonable values of params will be needed).  
Use XPP auto to produce a bifurcation diagram showing what happens as the flow rate  $F$  is gradually increased.